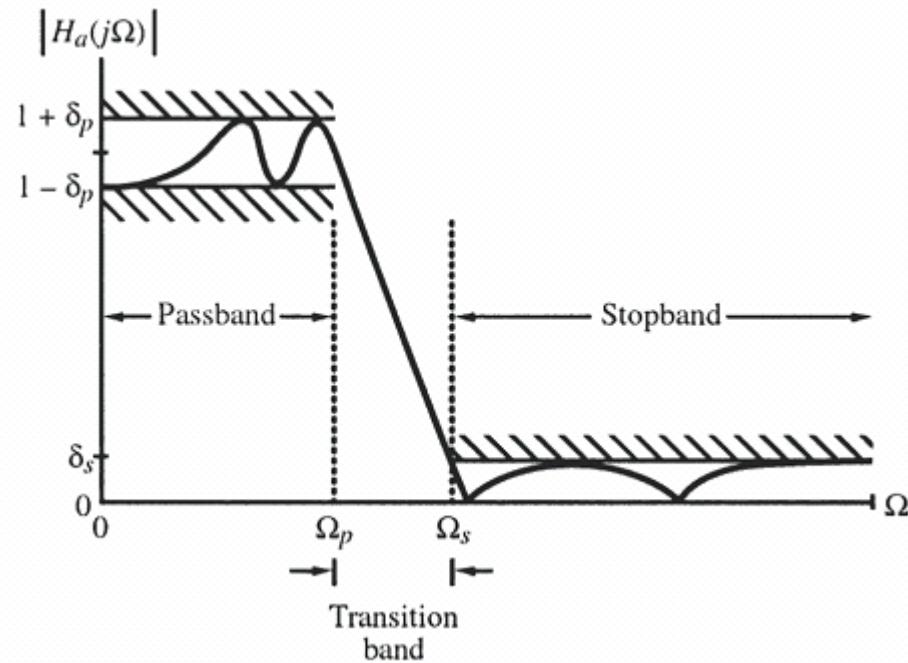
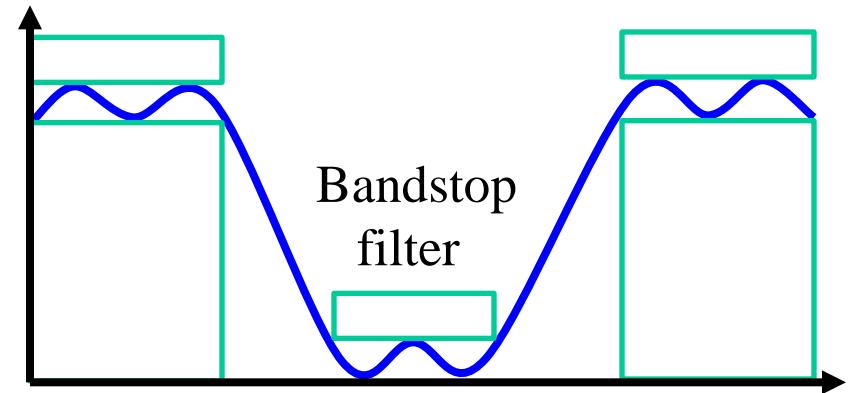
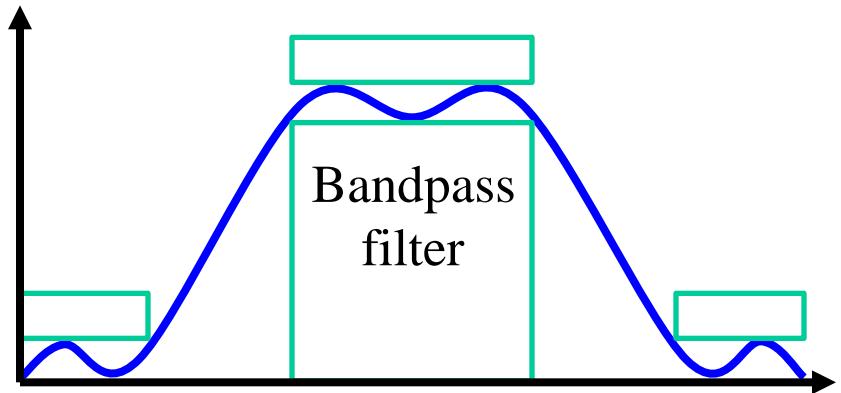
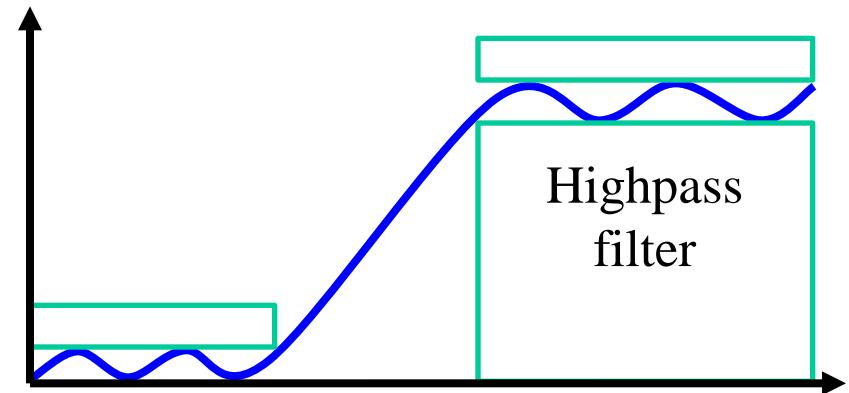
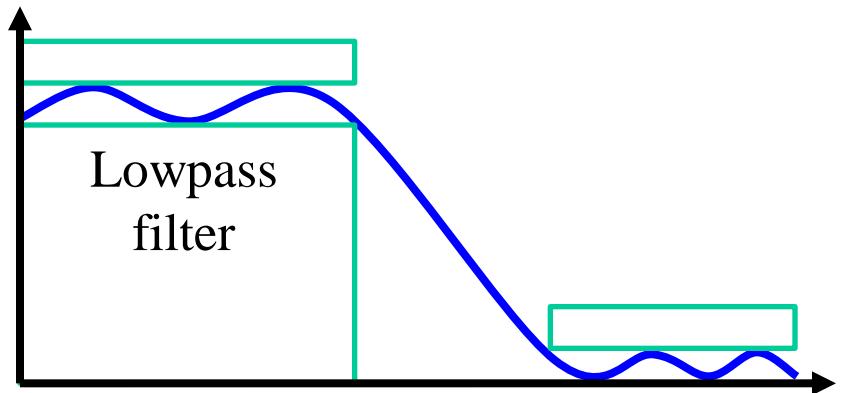


ELG4139: Active Filter Design

This simple filter is a kind of integrator, in which the capacitor integrates the charge provided through the resistor.

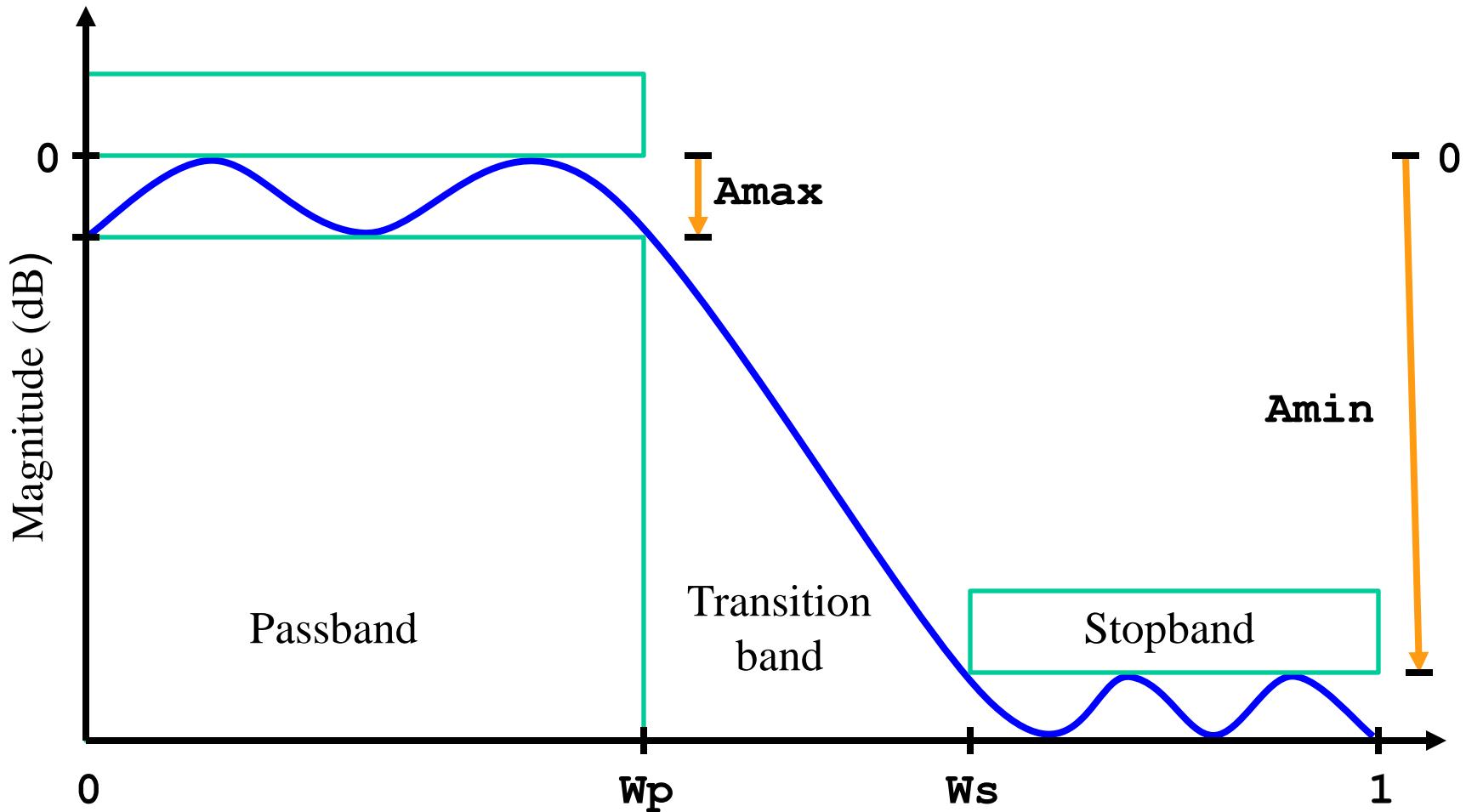


Filter Configurations

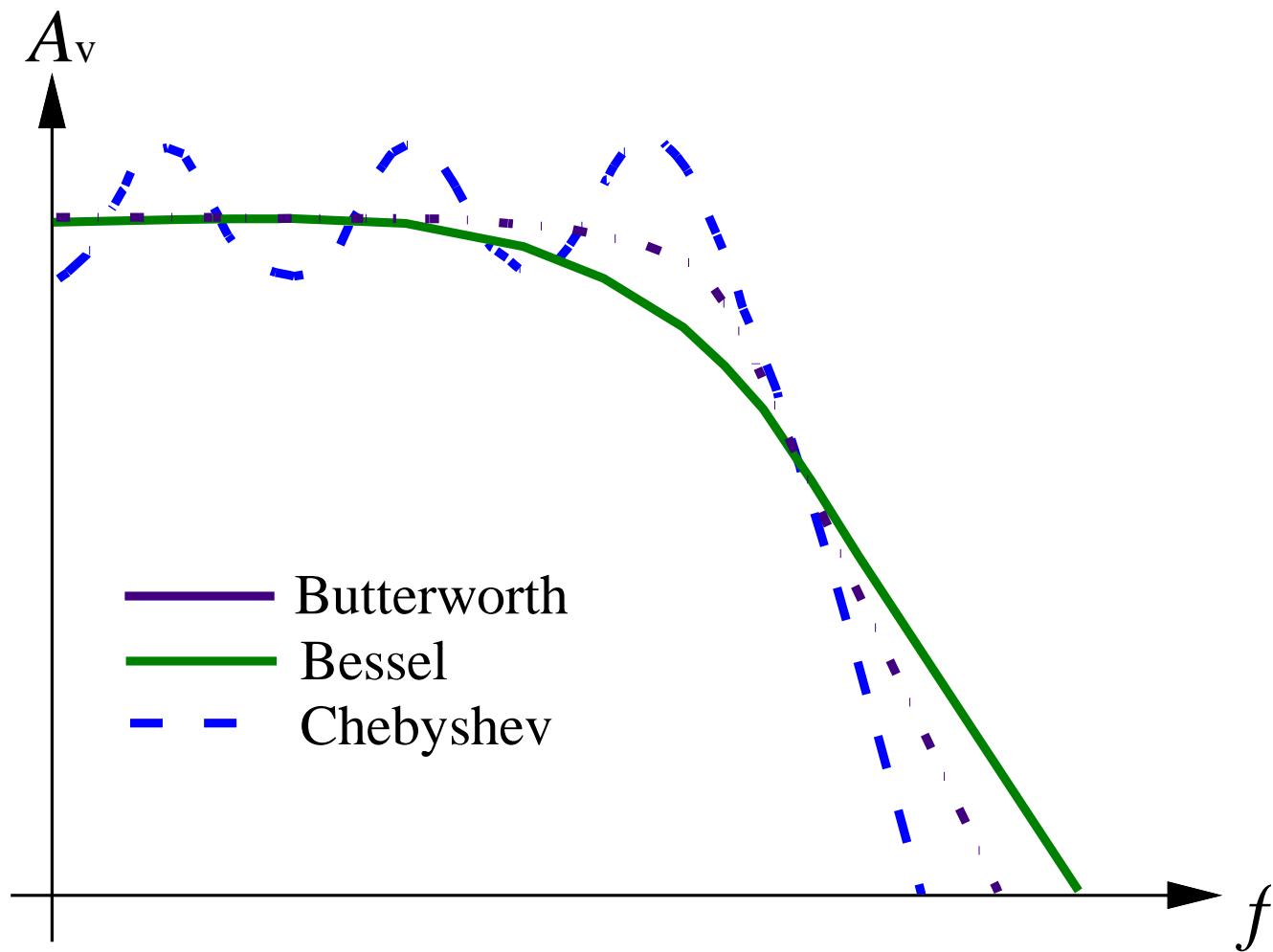


Normalization convention: $0 \leq f \leq 1$ = Nyquist frequency

Filter Specifications

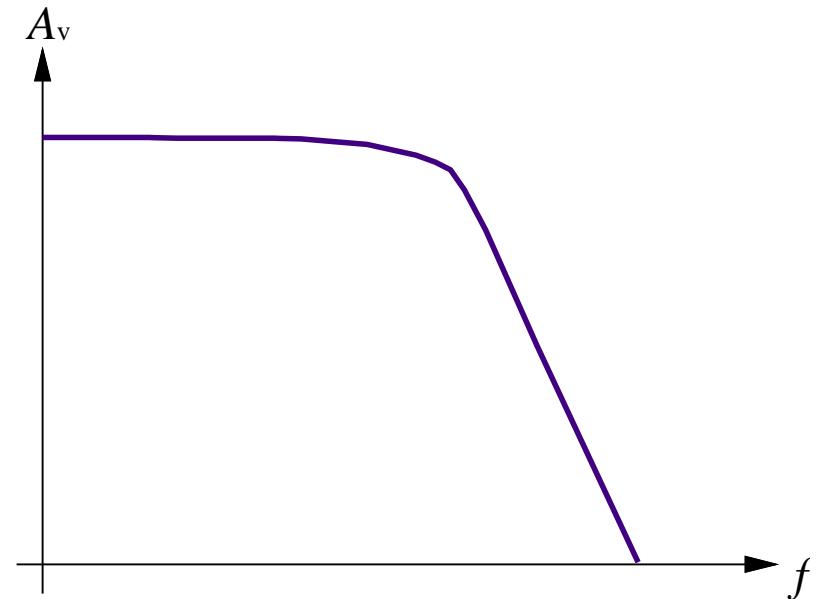


Filter Response Characteristics



Butterworth Characteristic

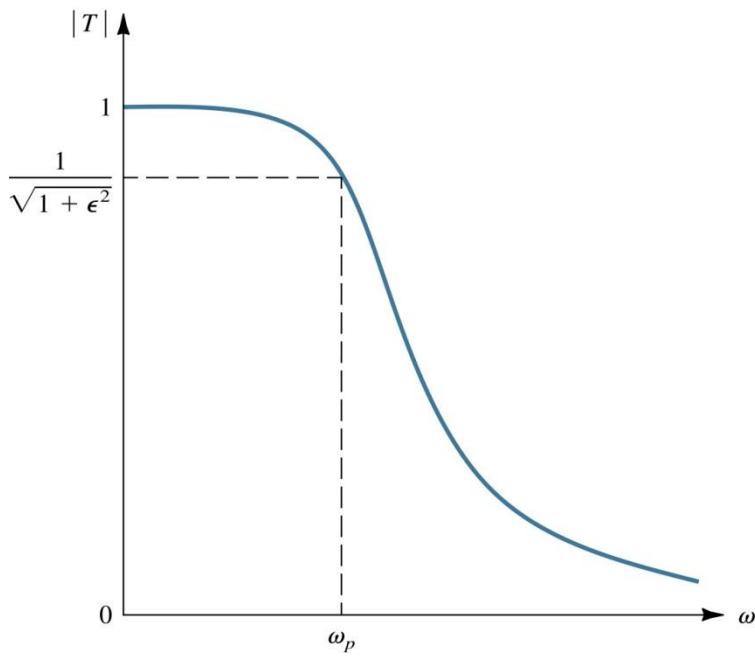
- Very flat amplitude, $A_{v(\text{dB})}$ response in the pass-band.
- Roll-off rate is 20dB/decade/pole.
- Phase response is not linear.
- Used when all frequencies in the pass-band must have the same gain.
- Often referred to as a maximally flat response.



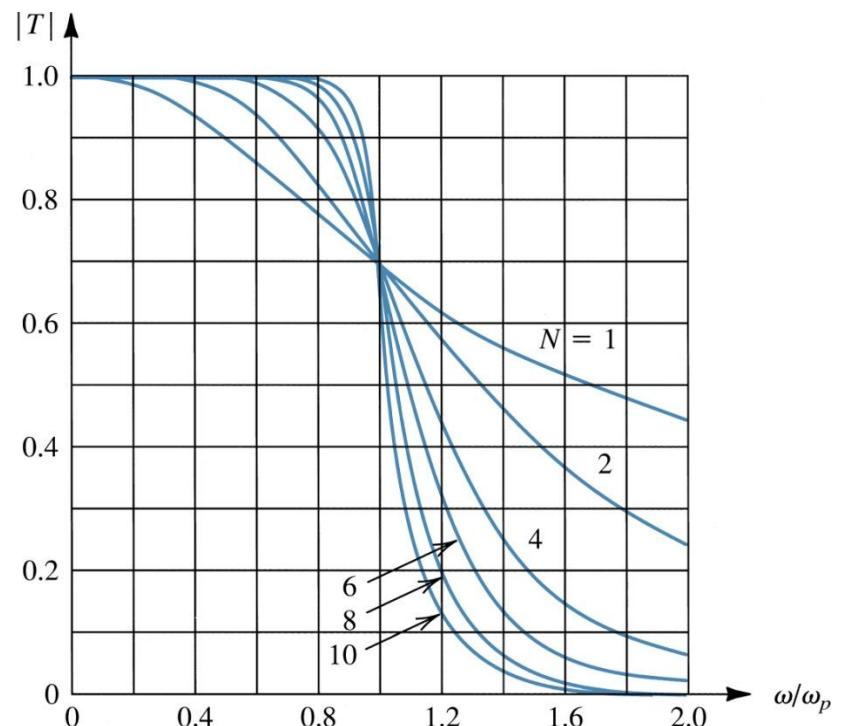
Design Criteria

- Requirements of a Customer:
 - A_{\max}
 - A_{\min} ;
 - Selectivity = $\frac{w_s}{w_p}$
- Find Number of Stages N
- Select the Configuration (for example Butterworth)
- Draw the Circuit and Find its Transfer Function
- Write the Standard Transfer Function
- Equate both Transfer Functions and Compare the Appropriate Sections to Find Values of Parameters Basing on the Quantities Given: Q and w .

Butterworth Filters



The magnitude response of a Butterworth filter.



Magnitude response for Butterworth filters of various order with $\epsilon = 1$. Note that as the order increases, the response approaches the ideal brickwall type transmission.

Finding Order of the Filter N

$$A(\omega_s) = 10 \log \left[1 + \varepsilon^2 \left(\frac{\omega_s}{\omega_p} \right)^{2N} \right] = A_{\min}$$

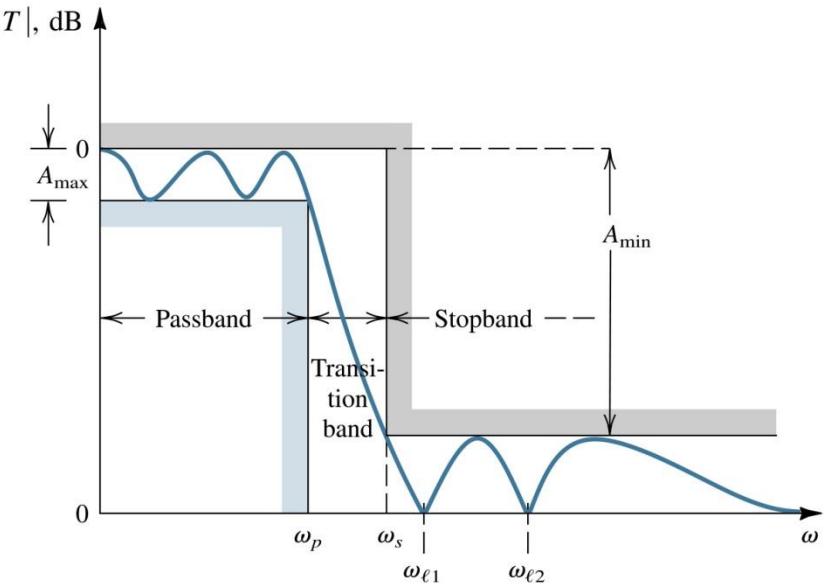
$$1 + \varepsilon^2 \left(\frac{\omega_s}{\omega_p} \right)^{2N} = 10^{\frac{A_{\min}}{10}}$$

$$\left(\frac{\omega_s}{\omega_p} \right)^{2N} = \frac{10^{\frac{A_{\min}}{10}} - 1}{\varepsilon^2}$$

$$\log \left[\left(\frac{\omega_s}{\omega_p} \right)^{2N} \right] = \log \left[\frac{10^{\frac{A_{\min}}{10}} - 1}{\varepsilon^2} \right]$$

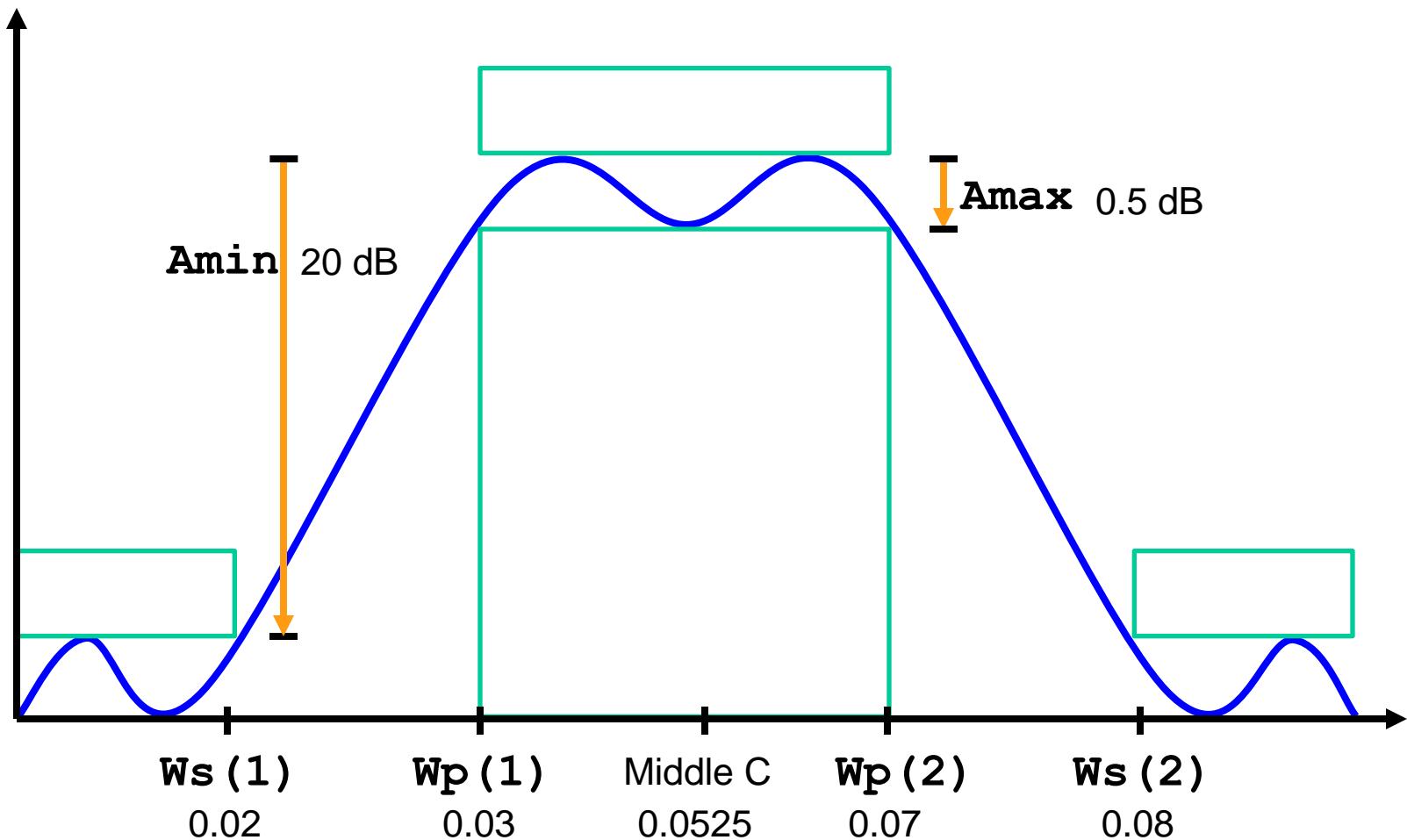
$$N = \frac{\log \left[\frac{10^{\frac{A_{\min}}{10}} - 1}{\varepsilon^2} \right]}{\log \left[\left(\frac{\omega_s}{\omega_p} \right)^2 \right]}$$

$$\varepsilon = \sqrt{10^{\frac{A_{\max}}{10}} - 1}$$



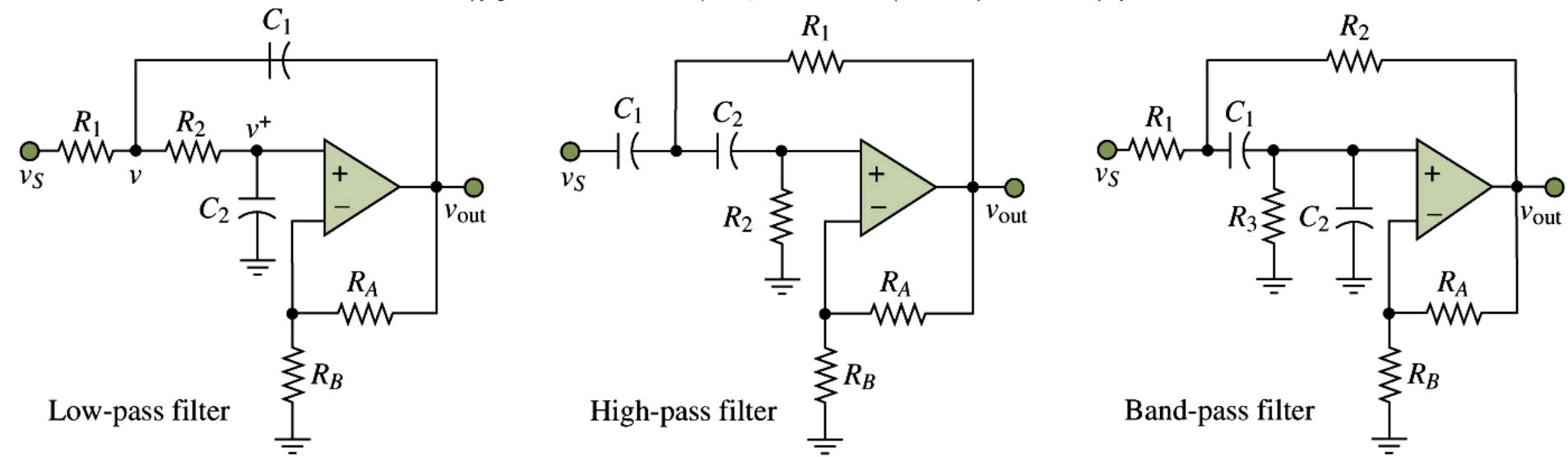
Example: Bandpass Filter

Order $N \leq 10$, sampling frequency $f_s = 10,000$ Hz

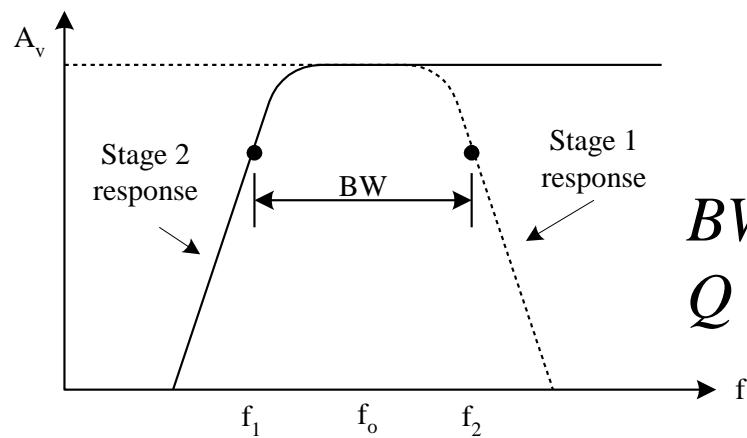
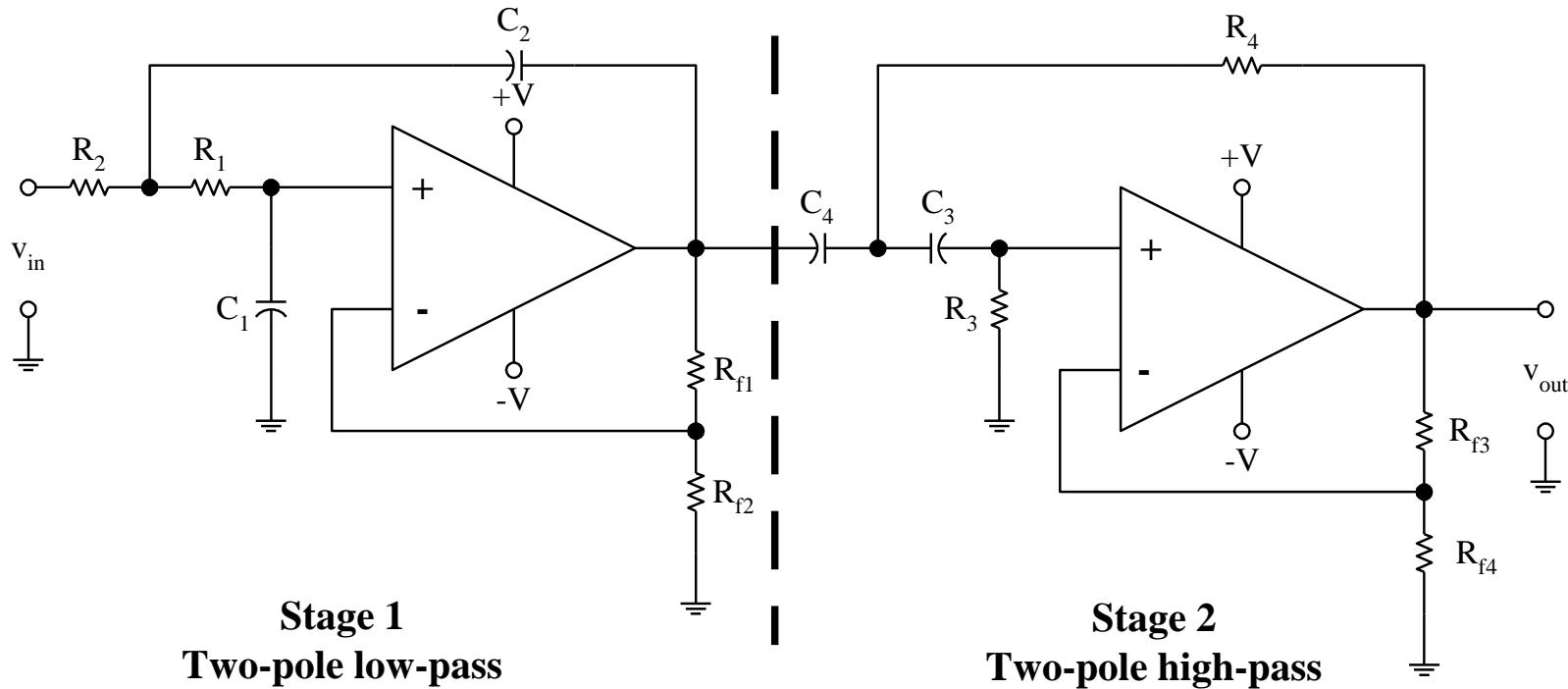


Sallen and Key Active Filters

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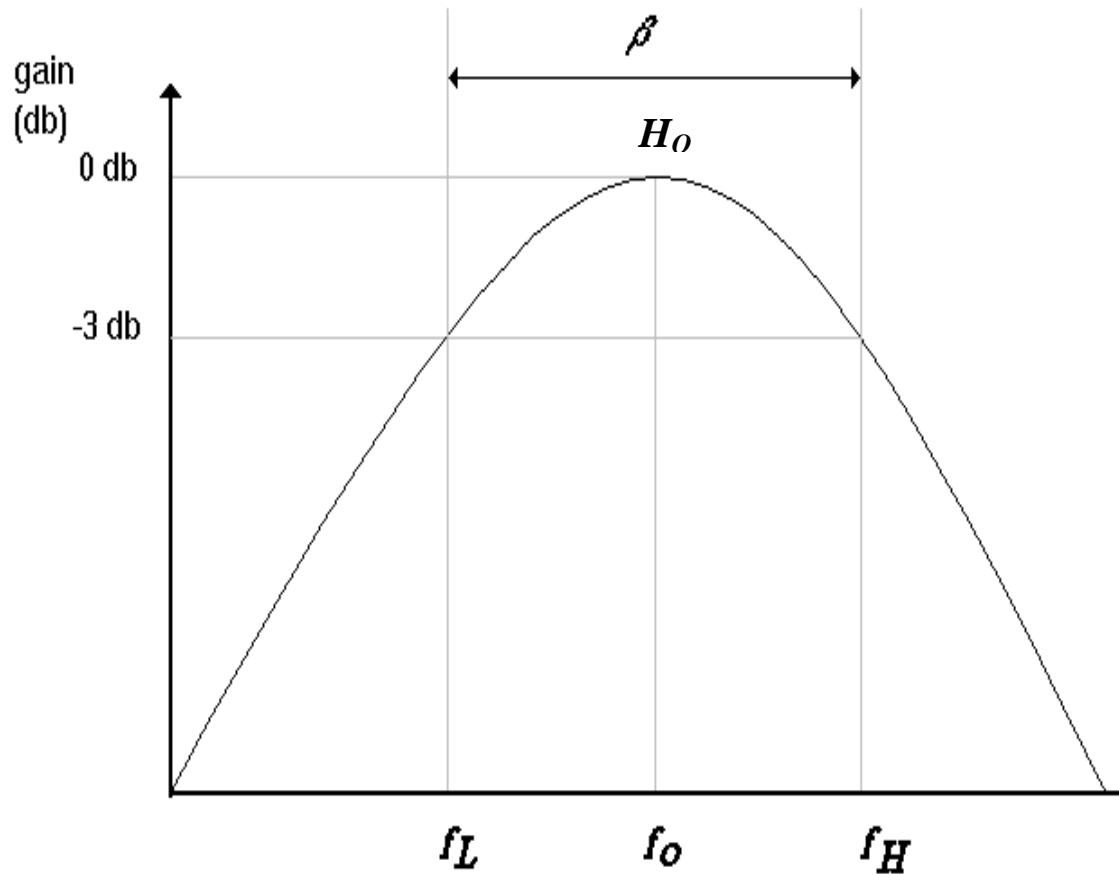


Two-Stage Band-Pass Filter: $N = 4$

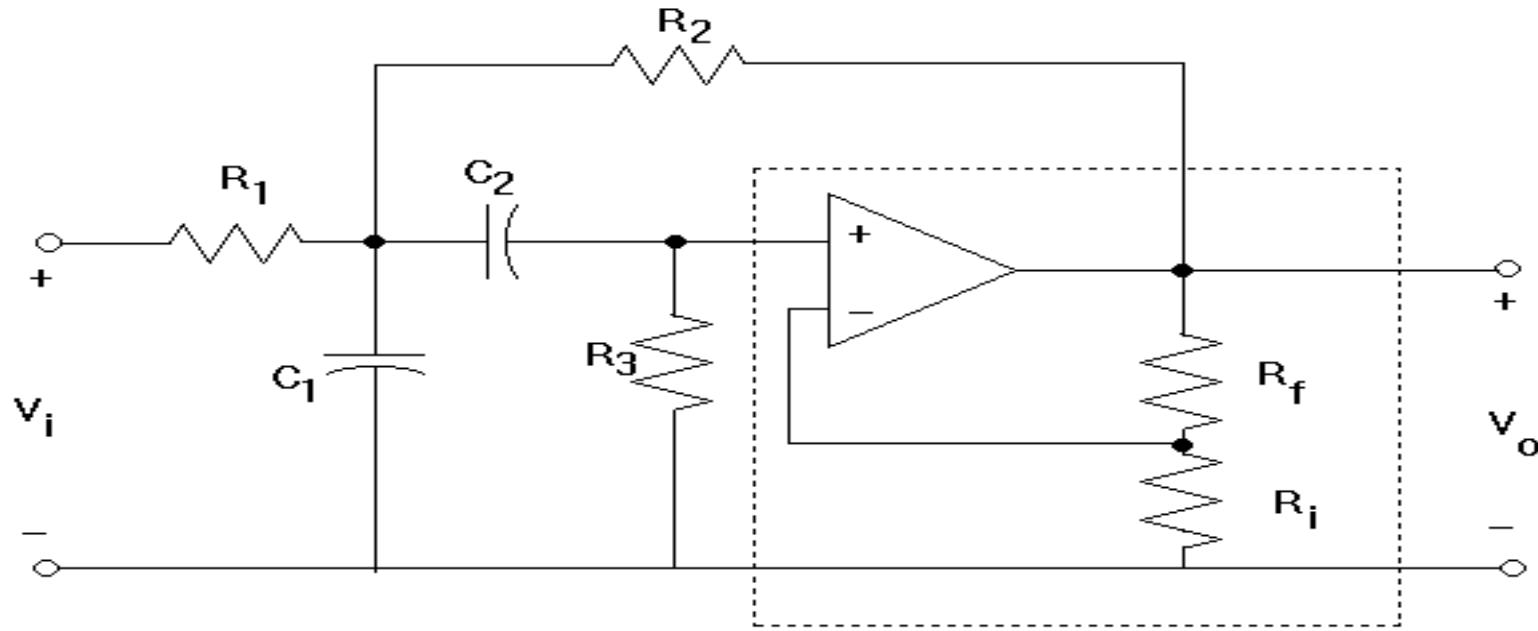


Band-Pass Filter Performance

- Quality Factor $Q = f_o / \beta$
 - Dimensionless figure of merit used to measure the selectivity of a filter expressed as ratio of center frequency to bandwidth



Design of Second Order Sallen-Key Band-Pass Filter



$$T(s) = \frac{V_o}{V_i} = \frac{\frac{Ks}{R_1 C_1}}{s^2 + \left(\frac{1}{R_1 C_1} + \frac{1}{R_3 C_1} + \frac{1}{R_3 C_2} + \frac{1-K}{R_2 C_1} \right) s + \frac{R_1 + R_2}{R_1 R_2 R_3 C_1 C_2}} \quad (2)$$

$$K = \frac{V_o}{V_x} = 1 + \frac{R_f}{R_i} \quad (1)$$

Equal Component Sallen-Key Filter

$$R_1 = R_2 = \frac{R_3}{2} = R \text{ and } C_1 = C_2 = C \quad (3)$$

$$T(s) = \frac{\frac{Ks}{RC}}{s^2 + \left(\frac{3-K}{RC}\right)s + \left(\frac{1}{RC}\right)^2} \quad (4)$$

$$s_{1,2} = \frac{-\left(\frac{3-K}{RC}\right) \pm \sqrt{\left(\frac{3-K}{RC}\right)^2 - 4\left(\frac{1}{RC}\right)^2}}{2} \quad (9)$$

In order to ensure stability of the filter, we must ensure that the poles of the transfer function lie in the left-half of the complex s-plane, or $\Re(s_{1,2}) < 0$. Thus, we must ensure that the gain of the op-amp is less than 3, i.e., $K < 3$.

Standard Second Order Filter

Compare (4) with (5)

$$T(s) = \frac{H_o \left(\frac{\omega_o}{Q} \right) s}{s^2 + \left(\frac{\omega_o}{Q} \right) s + \omega_o^2} \quad (5)$$

$$\omega_o = \frac{1}{RC}, \quad Q = \frac{1}{3-K}, \quad H_o = \frac{K}{3-K}$$

Note: For your design, let

$$R_1 = R_2 = \frac{R_3}{2} = R_i = 2k\Omega$$

Frequency Scaling

Frequency scaling is a method of changing a filter's frequency of operation

This method is extremely useful once one has designed a filter with a satisfactory response (i.e., ω_o , Q , and H_o) and then merely wants to change, for example, the center frequency

To increase the center frequency of a filter without affecting any of its other characteristics (i.e., Q and H_o), we can simply divide all frequency determining capacitors *or* divide all frequency determining resistors by the desired scaling factor

As an example, to triple the center frequency, divide all capacitor values by 3 *or* divide all resistor values by 3

Design of Fifth Order Butterworth Low Pass Filter

Design a fifth order Butterworth low pass filter with a gain (μ) of 1 and a cutoff frequency 10 kHz.

The normalized Butterworth low pass filter equation is:

$$\frac{V_2(s)}{V_1(s)} = H(s) = \frac{\mu}{R_1 R_2 C_1 C_2 s^2 + (R_1 C_1 + R_1 C_2 + R_2 C_2 - \mu R_1 C_1) s + 1}$$

For a gain (μ) of 1

$$\frac{V_2(s)}{V_1(s)} = H(s) = \frac{1}{R_1 R_2 C_1 C_2 s^2 + (R_1 C_1 + R_1 C_2 + R_2 C_2 - (1)^* R_1 C_1) s + 1}$$

For frequency scaling: Replace
 s with s/w_c

$$\frac{V_2(s)}{V_1(s)} = H(s) = \frac{1}{R_1 R_2 C_1 C_2 s^2 + (R_1 C_2 + R_2 C_1)s + 1}$$

The normalized denominator for the fifth order Butterworth low pass filter is:

$$H(s) = \frac{1}{(s+1)(s^2 + 0.618s + 1)(s^2 + 1.618s + 1)}$$

Diagram illustrating the stages of the filter:

- Stage 1: First order filter (s + 1)
- Stage 2: Second order filter ($s^2 + 0.618s + 1$)
- Stage 3: Second order filter ($s^2 + 1.618s + 1$)

Stage 1: First Order Filter

Assume the resistor in the design as $1 \text{ k}\Omega$.

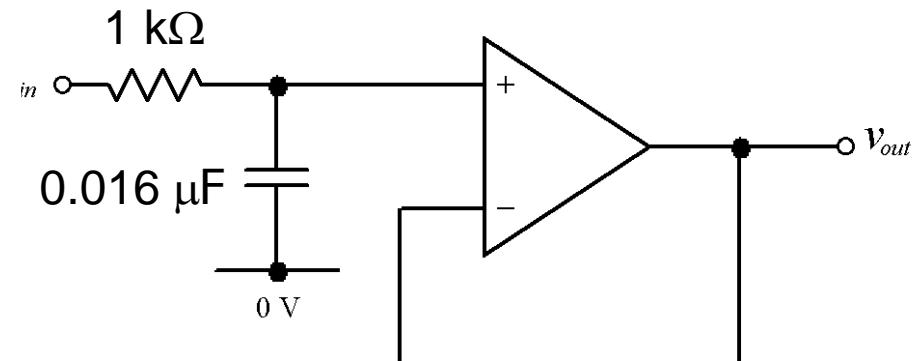
$$\frac{v_{out}}{v_{in}} = \frac{1/RC}{s + 1/RC}$$

$$\frac{v_{out}}{v_{in}} = \frac{1/RC}{s/20000\pi + 1/RC}$$

$$1/RC = \omega_c = 20000\pi$$

$$(1000 \times C) = \frac{1}{20000\pi}$$

$$C = \frac{1}{(1000 \times 20000)\pi} = 1.59 \times 10^{-8} \approx 0.016 \mu F$$



Stage 2 and 3: Second Order Filter

$$H(s) = \frac{1}{(s^2 + 0.618s + 1)}$$

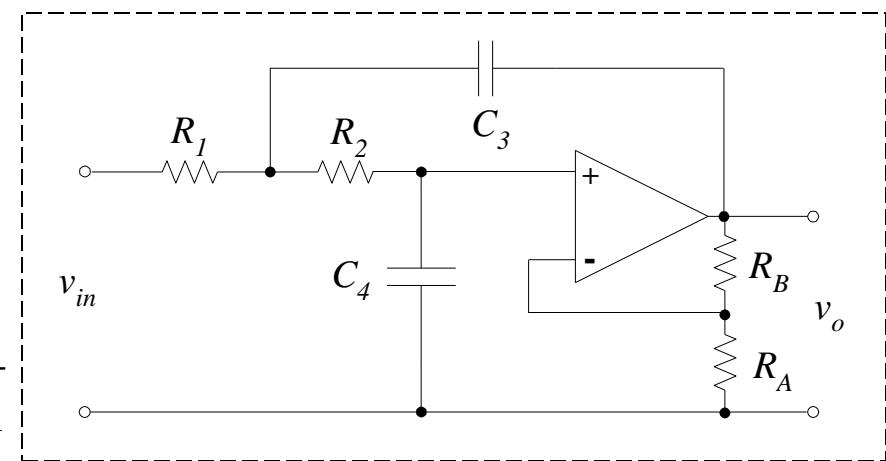
Defines one of the second order filters

$$H(s) = \frac{1}{\left(\frac{s^2}{(20000\pi)^2} + 0.618 \frac{s}{20000\pi} + 1 \right)}$$

$$H(s) = \frac{1}{R_1 R_2 C_1 C_2 s^2 + (R_1 C_2 + R_2 C_2)s + 1}$$

$$H(s) = \frac{1}{R_1 R_2 C_1 C_2 s^2 + (R_1 C_2 + R_2 C_2)s + 1}$$

$$H(s) = \frac{1}{(1000)^2 C_1 C_2 s^2 + 1000(C_1 + C_2)s + 1}$$



$$\frac{1}{(1000)^2 C_1 C_2 s^2 + 1000(2C_2)s + 1}$$

$$= \frac{1}{\frac{s^2}{(20000\pi)^2} + 0.618 \frac{s}{20000\pi} + 1}$$

$$1000(2C_2) = \frac{0.618}{20000\pi} \quad C_2 = \frac{0.618}{40000000\pi} = 0.0049 \mu F$$

$$(1000)^2 C_1 C_2 = \frac{1}{(20000\pi)^2}$$

$$C_1 = \frac{1}{(0.0049 \times 10^{-6})(1.0 \times 10^6)(20000\pi)^2}$$

$$C_1 = \frac{1}{0.0049(20000\pi)^2} = 5.17 \times 10^{-8} = 0.05 \mu F$$

$$H(s) = \frac{1}{(s^2 + 1.618s + 1)}$$

Defines the other second order filters

$$H(s) = \frac{1}{\left(\frac{s^2}{(20000\pi)^2} + 1.618 \frac{s}{20000\pi} + 1 \right)}$$

$$H(s) = \frac{1}{R_1 R_2 C_1 C_2 s^2 + (R_1 C_2 + R_2 C_1)s + 1}$$

$$H(s) = \frac{1}{(1000 \times 1000) C_1 C_2 s^2 + (1000 C_2 + 1000 C_1)s + 1}$$

$$H(s) = \frac{1}{(1000)^2 C_1 C_2 s^2 + 1000(C_1 + C_2)s + 1}$$

$$\begin{aligned}
& \frac{1}{(1000)^2 C_1 C_2 s^2 + 1000(2C_2)s + 1} \\
&= \frac{1}{\frac{s^2}{(20000\pi)^2} + 1.618 \frac{s}{20000\pi} + 1}
\end{aligned}$$

$$1000(2C_2) = \frac{1.618}{20000\pi} \quad C_2 = \frac{1.618}{40000000\pi} = 1.29 \times 10^{-8} = 0.013 \mu F$$

$$(1000)^2 C_1 C_2 = \frac{1}{(20000\pi)^2} \quad C_1 = \frac{1}{(0.013 \times 10^{-6})(1.0 \times 10^6)(20000\pi)^2}$$

$$C_1 = \frac{1}{0.013 \times (20000\pi)^2} = 1.95 \times 10^{-8} = 0.0195 \mu F$$